

Modeling elastic wave propagation in general anisotropic media

Bas Peters, December 4 , 2012

Elastic wave equation

σ :stress tensor, ρ :density, ω :frequency,
 u :displacement, f :force, x :spatial coordinate

$$-\frac{\partial \sigma_{i,j}}{\partial x_j} - \rho \omega^2 u_i = f_i$$

Hooke's law

In Voigt notation:

$$\begin{pmatrix} \sigma_{1,1} \\ \sigma_{2,2} \\ \sigma_{3,3} \\ \sigma_{2,3} \\ \sigma_{3,1} \\ \sigma_{1,2} \end{pmatrix} = \begin{pmatrix} C_{1,1} & C_{1,2} & C_{1,3} & C_{1,4} & C_{1,5} & C_{1,6} \\ C_{1,2} & C_{2,2} & C_{2,3} & C_{2,4} & C_{2,5} & C_{2,6} \\ C_{1,3} & C_{2,3} & C_{3,3} & C_{3,4} & C_{3,5} & C_{3,6} \\ C_{1,4} & C_{2,4} & C_{3,4} & C_{4,4} & C_{4,5} & C_{4,6} \\ C_{1,5} & C_{2,5} & C_{3,5} & C_{4,5} & C_{5,5} & C_{5,6} \\ C_{1,6} & C_{2,6} & C_{3,6} & C_{4,6} & C_{5,6} & C_{6,6} \end{pmatrix} \begin{pmatrix} \frac{\partial u_1}{\partial x_1} \\ \frac{\partial u_2}{\partial x_2} \\ \frac{\partial u_3}{\partial x_3} \\ \frac{\partial u_2}{\partial x_3} + \frac{\partial u_3}{\partial x_2} \\ \frac{\partial u_3}{\partial x_1} + \frac{\partial u_1}{\partial x_3} \\ \frac{\partial u_1}{\partial x_2} + \frac{\partial u_2}{\partial x_1} \end{pmatrix}$$

Set up of linear system

- Substitute Hooke's law into the wave equation and reorganize:

$$\begin{pmatrix} A_{1,1} - \rho\omega^2 & A_{1,2} & A_{1,3} \\ A_{2,1} & A_{2,2} - \rho\omega^2 & A_{2,3} \\ A_{3,1} & A_{3,2} & A_{3,3} - \rho\omega^2 \end{pmatrix} \begin{pmatrix} u_1 \\ u_2 \\ u_3 \end{pmatrix} = \begin{pmatrix} f_1 \\ f_2 \\ f_3 \end{pmatrix}$$

$$\rightarrow [\mathbf{A} - \rho\omega^2 \mathbf{I}] \mathbf{u} = \mathbf{f}$$

- $A_{i,j}$ terms contain stiffness tensor components and spatial derivatives

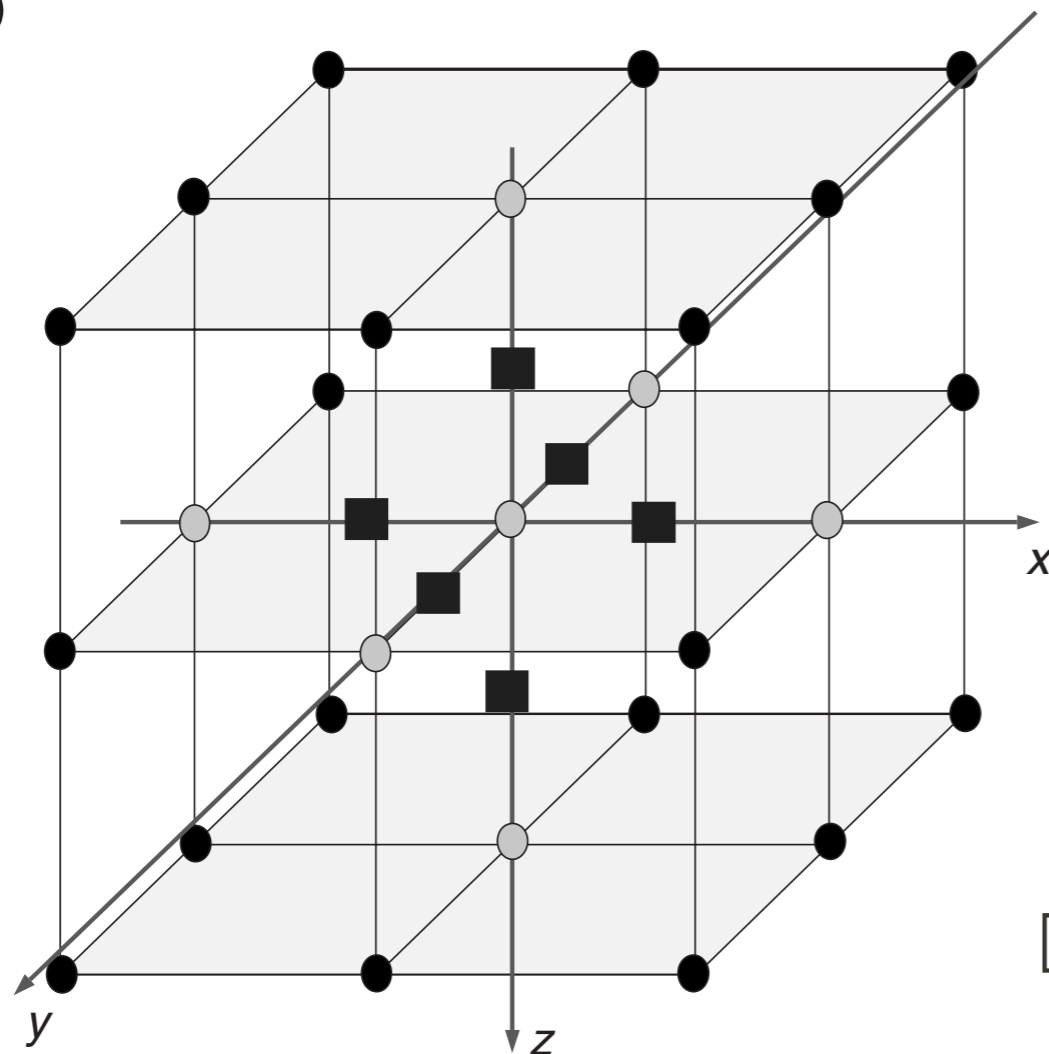
Discretization

- 2nd order centred differences on 8 different coordinate systems
- This decreases the numerical dispersion and numerical anisotropy

Visualization of coordinates

- 1 Cartesian grid

a)

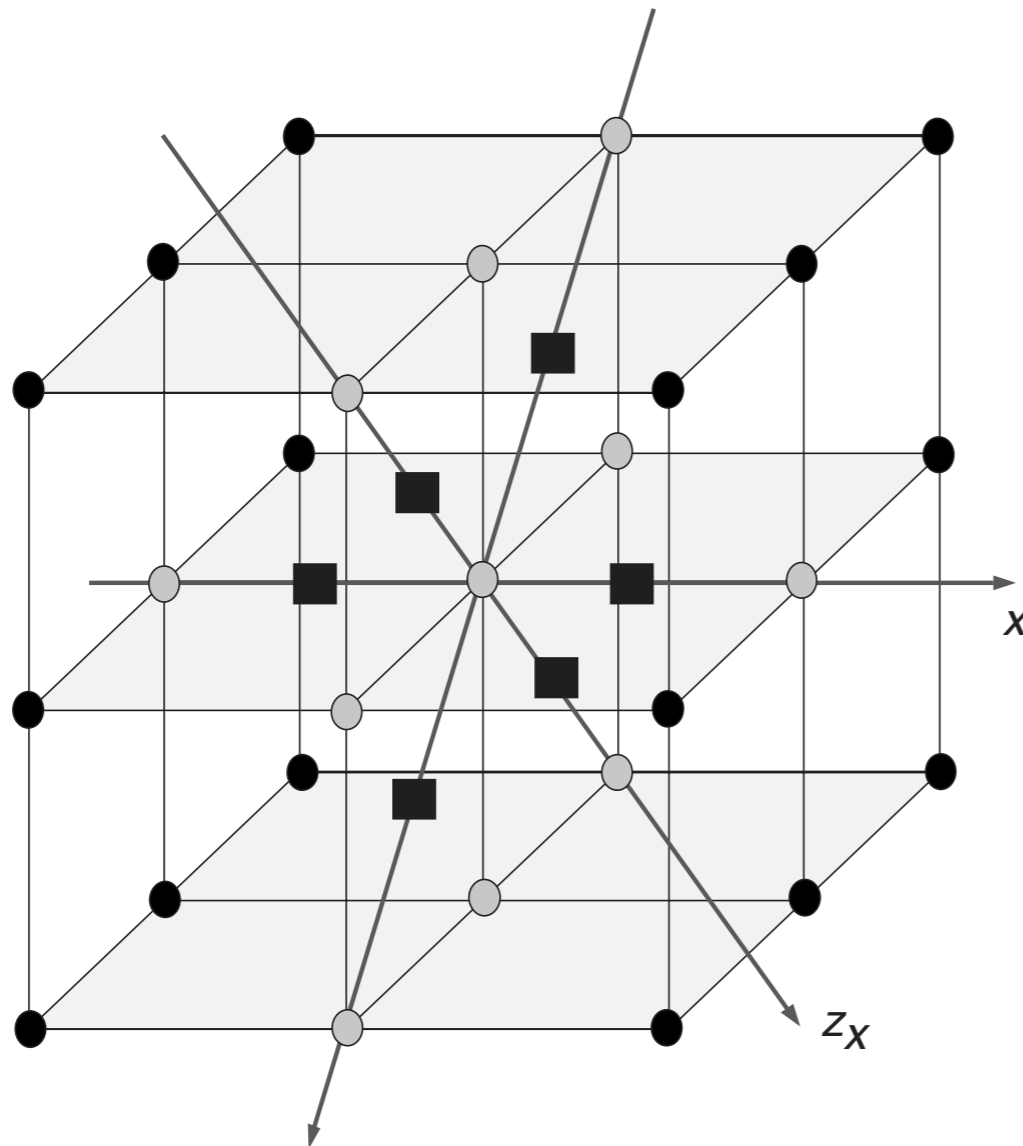


[from Operto et al., 2007]

Visualization of coordinates

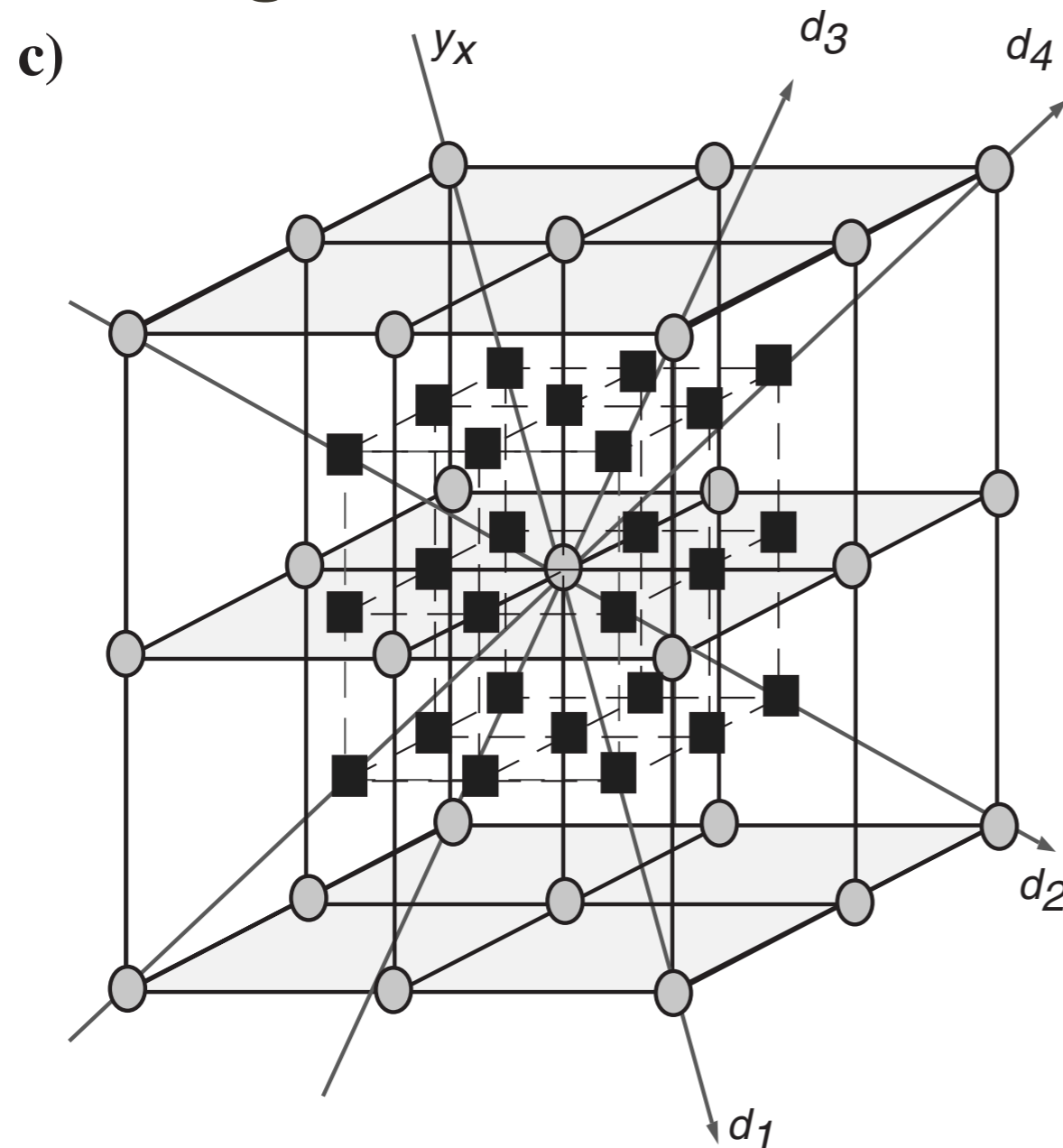
- 3 coordinate systems by rotating about each of the cartesian axis

b)



Visualization of coordinates

- 4 coordinate systems formed by 3 different diagonals of a cube



Mass lumping

- Improve accuracy by distributing the mass over grid points surrounding the grid point under consideration

Linear combination of grids

$$\mathbf{A} = w_1 \mathbf{A}_c + \frac{w_2}{3} (\mathbf{A}_1 + \mathbf{A}_2 + \mathbf{A}_3) + \frac{w_3}{4} (\mathbf{A}_{d1} + \mathbf{A}_{d2} + \mathbf{A}_{d3} + \mathbf{A}_{d4})$$

- c : Cartesian; 1,2 and 3 : rotated coordinate systems; d_1, d_2, d_3, d_4 : diagonal coordinate systems
- Estimate weights (w) by global optimization
- Results in 5 grid points per smallest wavelength

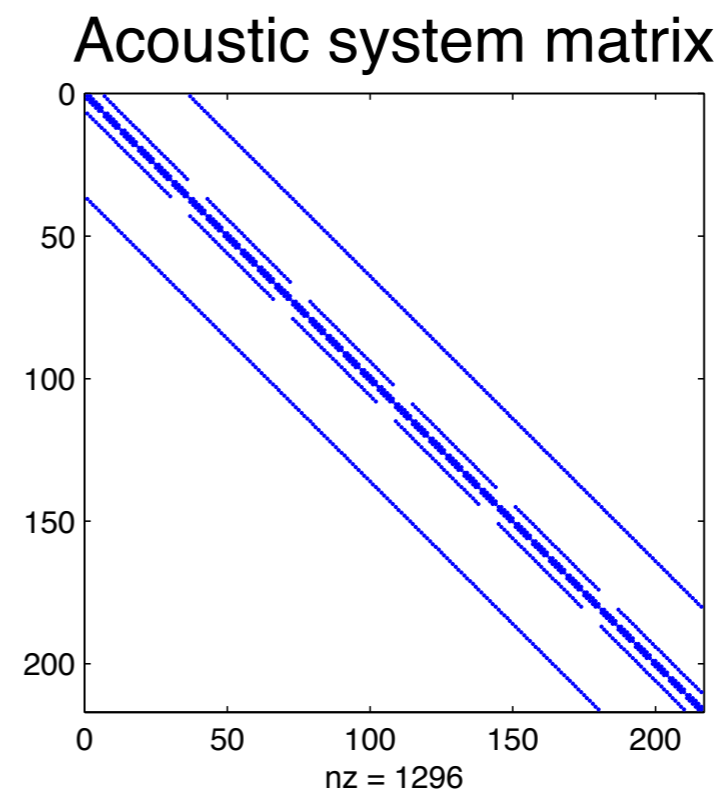
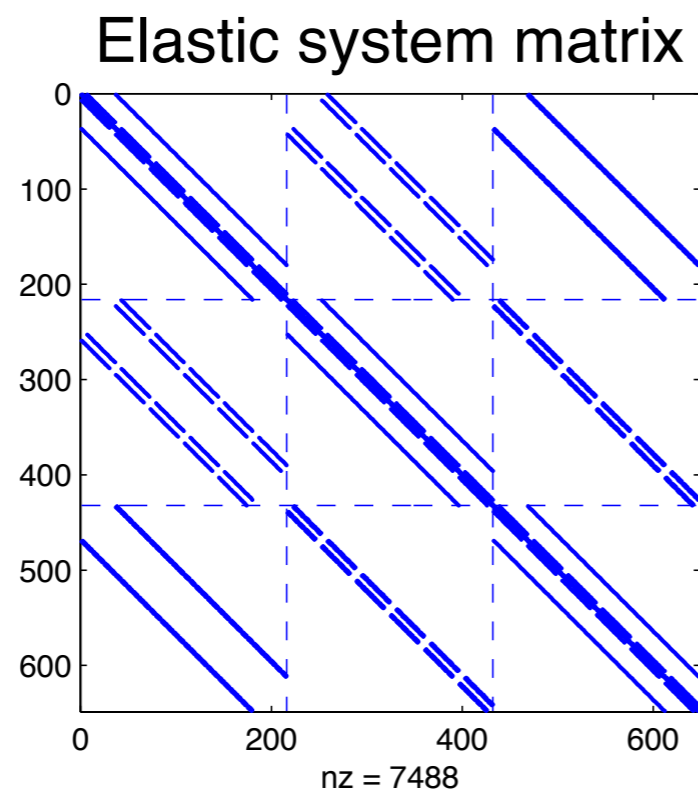
Stiffness tensor approximations

- In case modeling or estimation of all 21 components is not desired
- Example: orthorhombic symmetry:

$$\begin{pmatrix} C_{1,1} & C_{1,2} & C_{1,3} & C_{1,4} & C_{1,5} & C_{1,6} \\ C_{1,2} & C_{2,2} & C_{2,3} & C_{2,4} & C_{2,5} & C_{2,6} \\ C_{1,3} & C_{2,3} & C_{3,3} & C_{3,4} & C_{3,5} & C_{3,6} \\ C_{1,4} & C_{2,4} & C_{3,4} & C_{4,4} & C_{4,5} & C_{4,6} \\ C_{1,5} & C_{2,5} & C_{3,5} & C_{4,5} & C_{5,5} & C_{5,6} \\ C_{1,6} & C_{2,6} & C_{3,6} & C_{4,6} & C_{5,6} & C_{6,6} \end{pmatrix} \approx \begin{pmatrix} C_{1,1} & C_{1,2} & C_{1,3} & 0 & 0 & 0 \\ C_{1,2} & C_{2,2} & C_{2,3} & 0 & 0 & 0 \\ C_{1,3} & C_{2,3} & C_{3,3} & 0 & 0 & 0 \\ 0 & 0 & 0 & C_{4,4} & 0 & 0 \\ 0 & 0 & 0 & 0 & C_{5,5} & 0 \\ 0 & 0 & 0 & 0 & 0 & C_{6,6} \end{pmatrix}$$

Sparsity pattern of the system

- 81 point stencil and large bandwidth



- Grid: $N=(n1 \times n2 \times n3)$
- Acoustic system = $N \times N$, Elastic system = $3 (N \times N)$

System matrix permutations

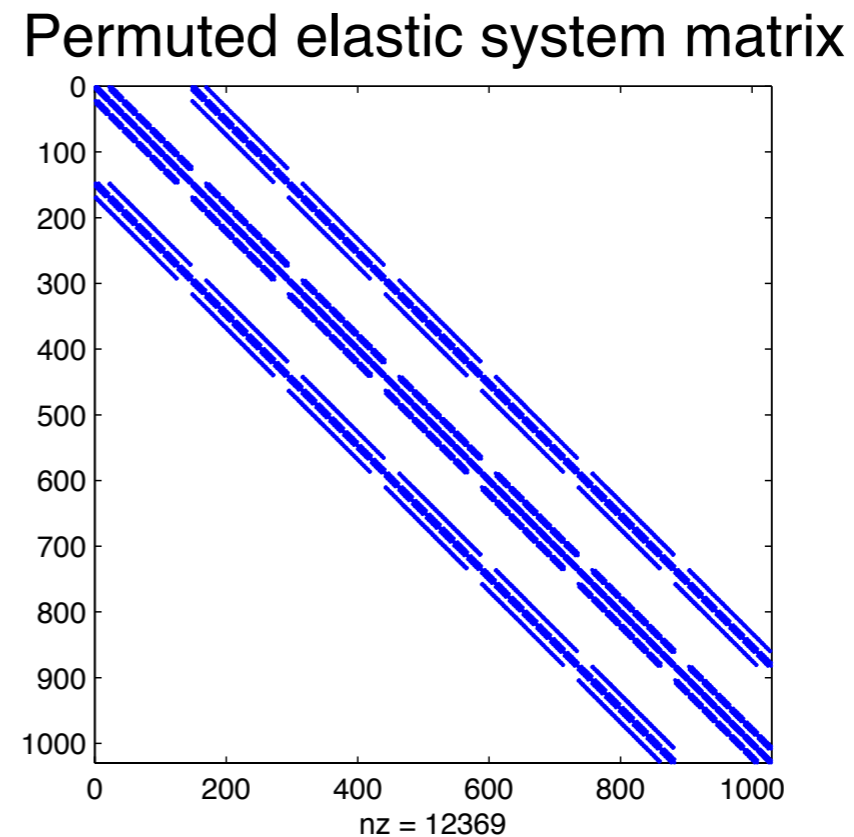
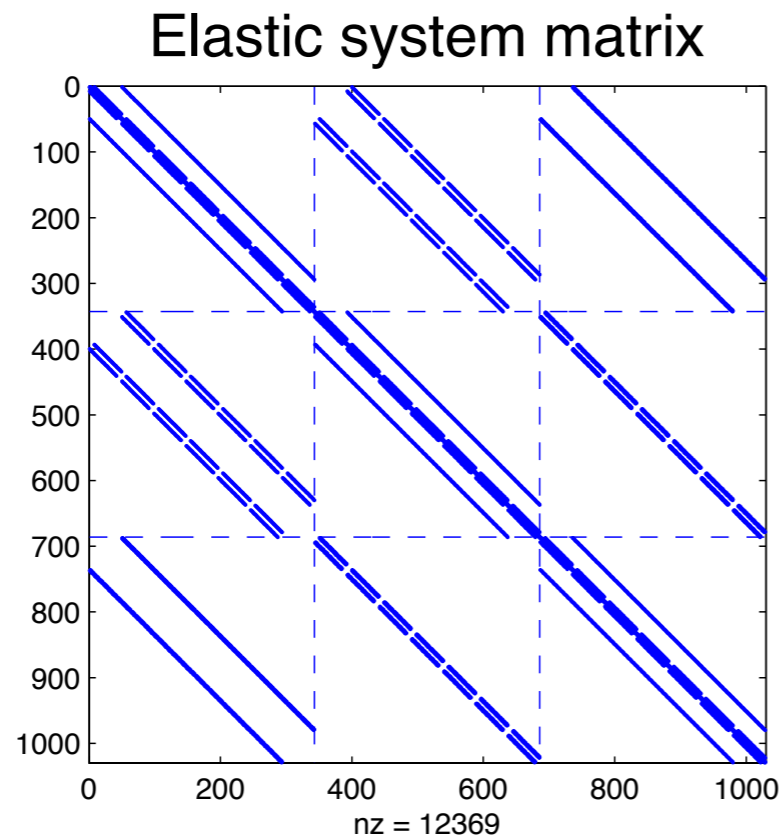
- 1) Permute rows of A and f
- 2) Permute columns of A and u (implicit)

P_r/P_c : row/column permutation matrix

$$P_r [A - \rho\omega^2 I] P_c P_c u = P_r f$$

System matrix permutations

- Bandwidth is decreased a lot
- Useful for direct solvers



Eigenvalues

- Convergence of iterative solvers generally depends on the condition number and eigenvalue clustering
- Matrix permutation does not change the condition number, but changes the eigenvalues
- Interested in eigenvalue clustering after preconditioning, because the system matrix is indefinite

Eigenvalues

- Elastic condition number is much larger than the acoustic one
- Anisotropy can increase the condition number
- Effective preconditioner required to cluster eigenvalues/lower condition number

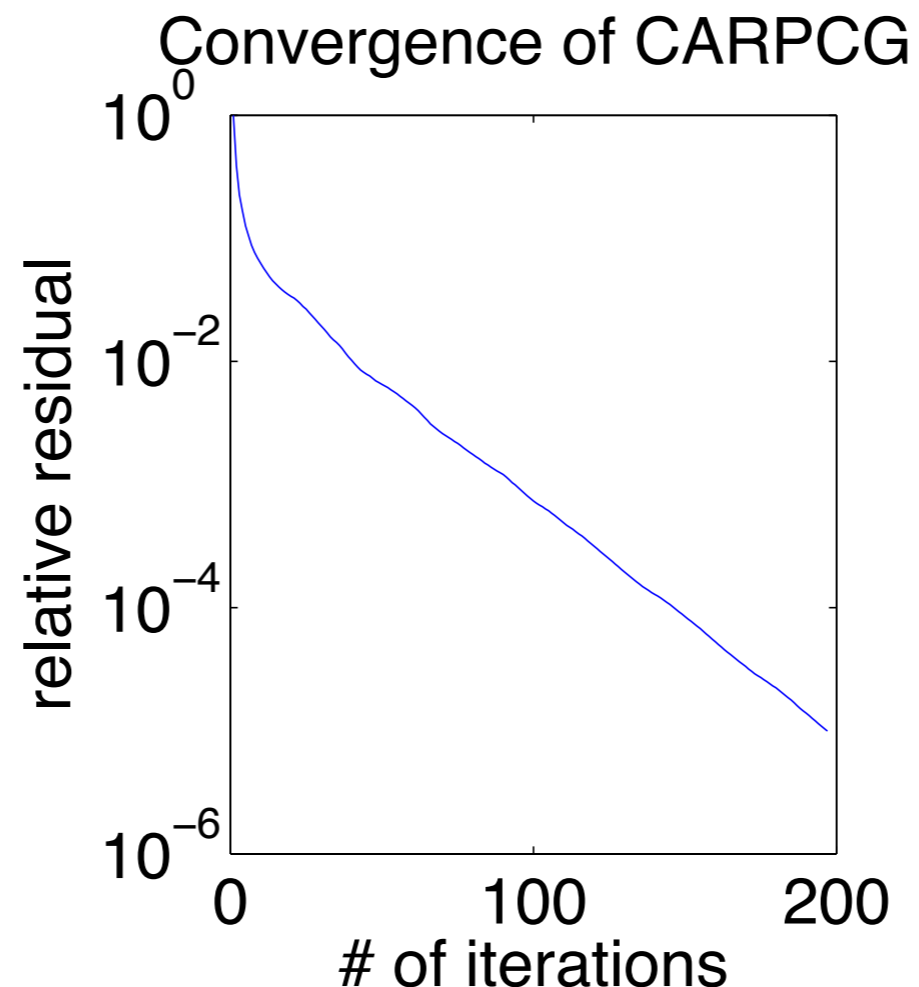
Solving the system

- At the moment, solve iteratively with preconditioning on CPU's
- CARPCG is currently used

Result using CARPCG

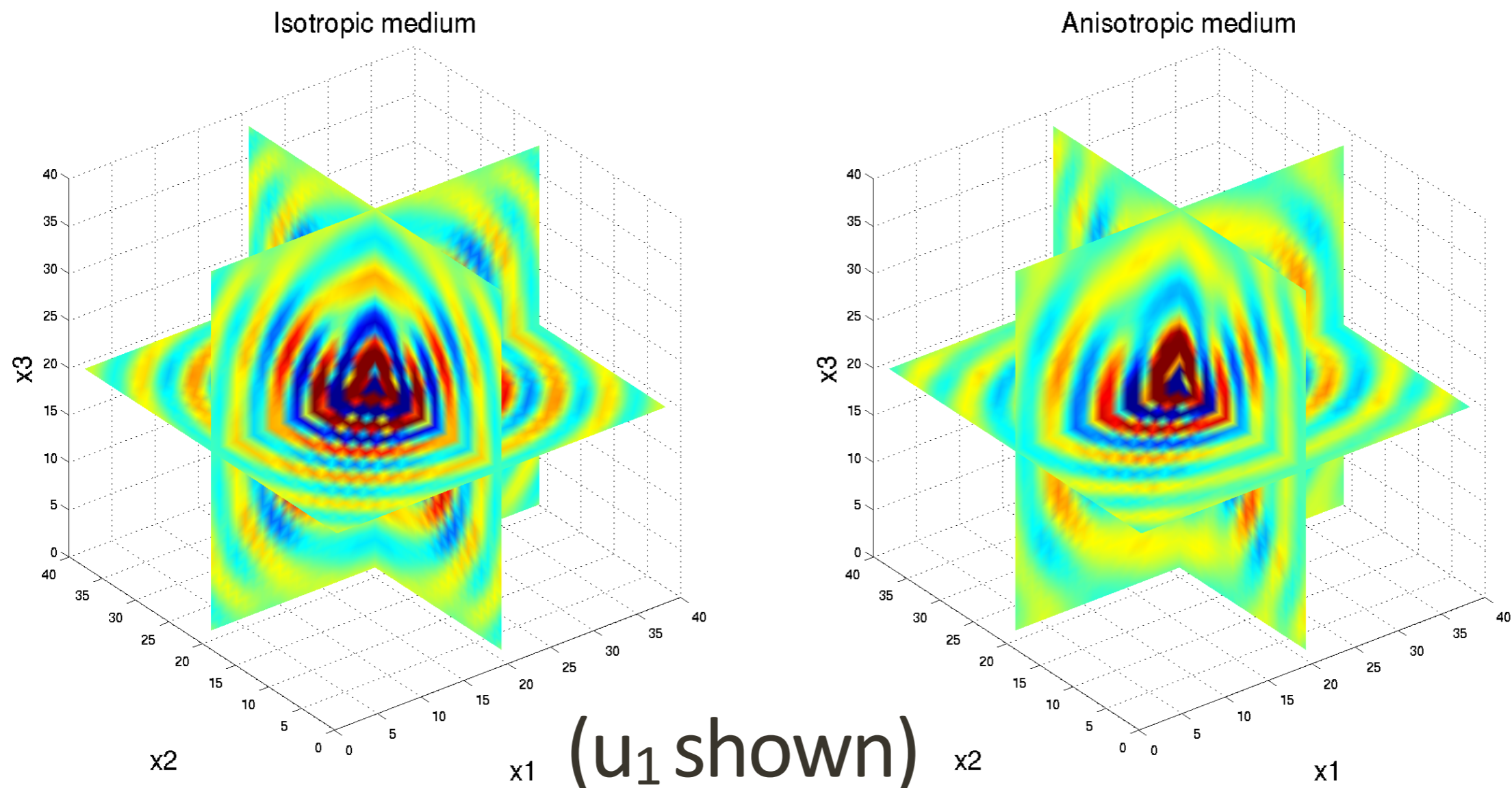
Consider (if applicable):

- Overhead cost of forming the preconditioner
- Extra matrix operations each iteration
- Number of right hand sides
- Grid size



Some results

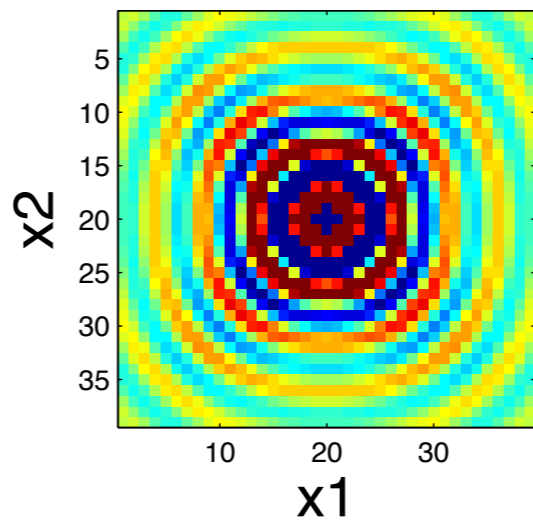
- Point force source at the center of the domain
- Energy loss and stiffness tensor are anisotropic
- Homogeneous medium with PML



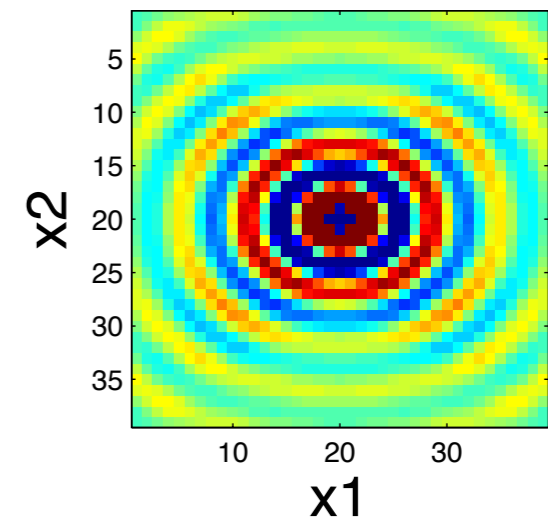
Cross sections from previous figure

U_1 component (real part)

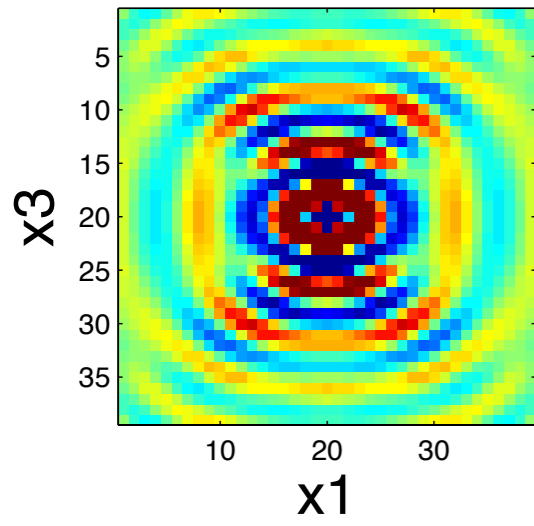
Isotropic medium



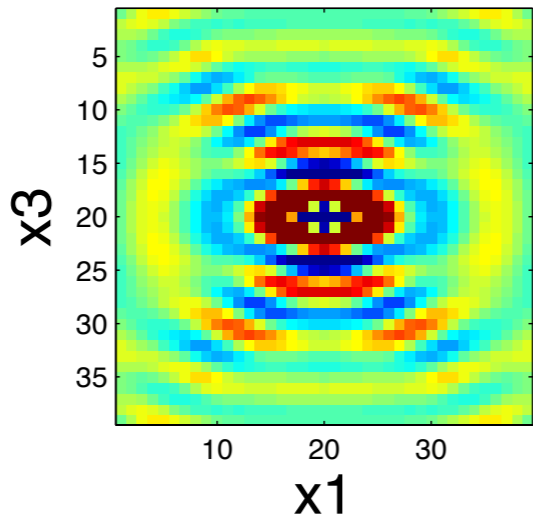
Anisotropic medium



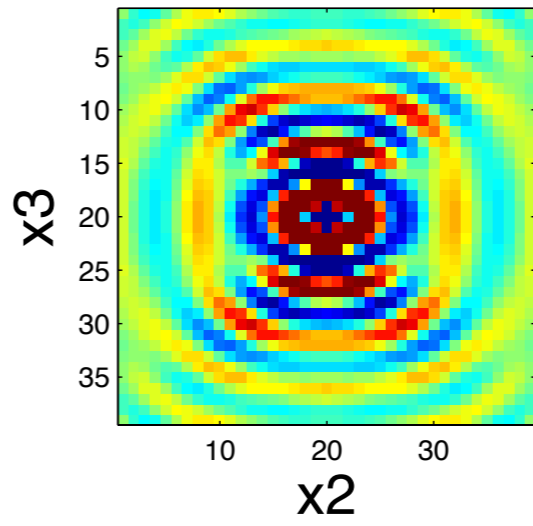
Isotropic medium



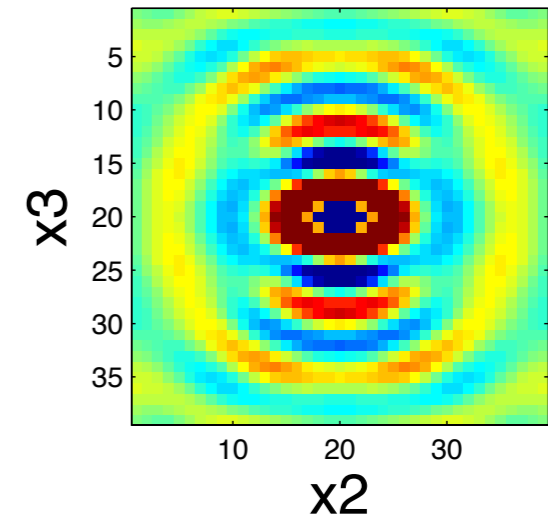
Anisotropic medium



Isotropic medium

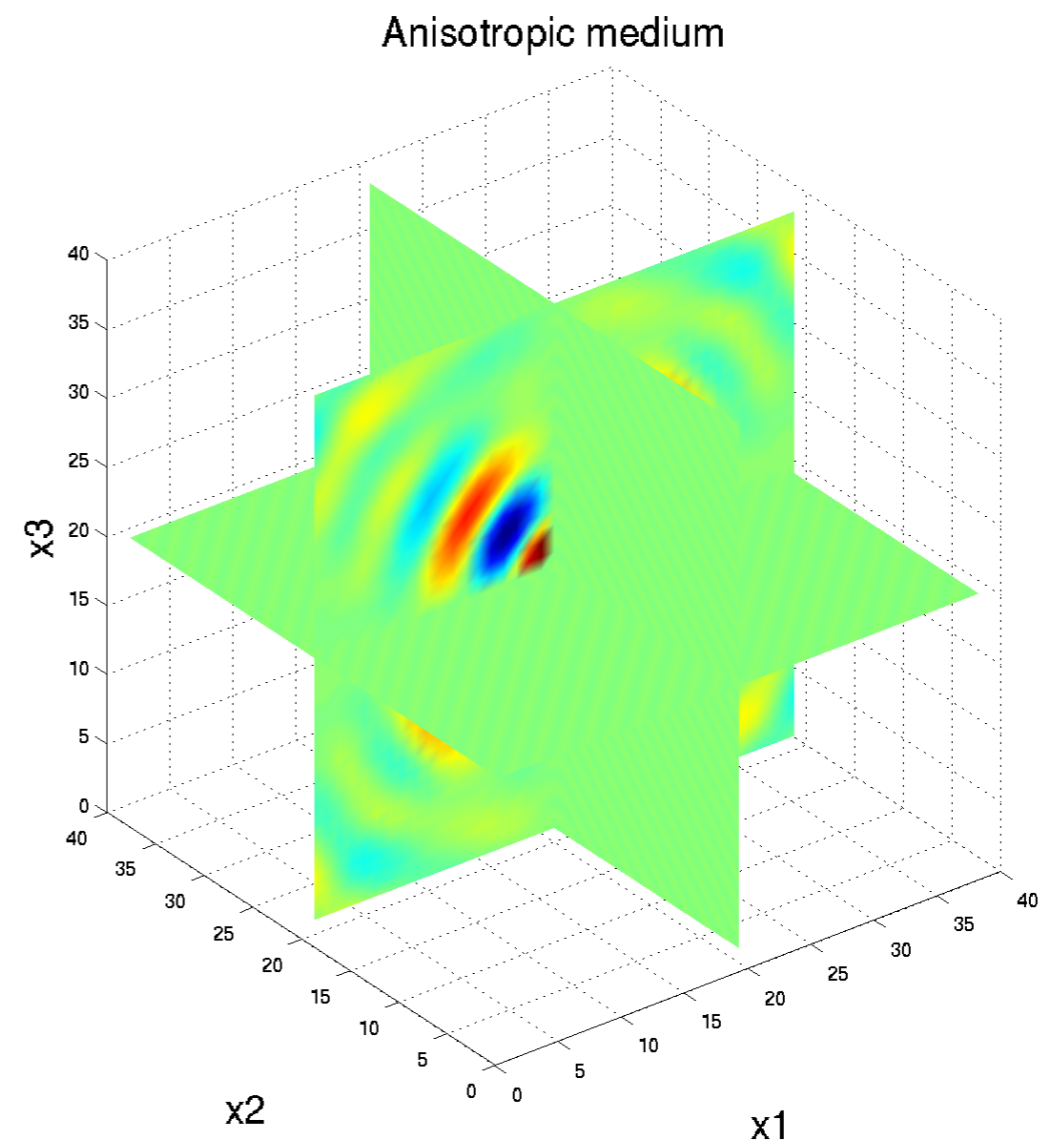
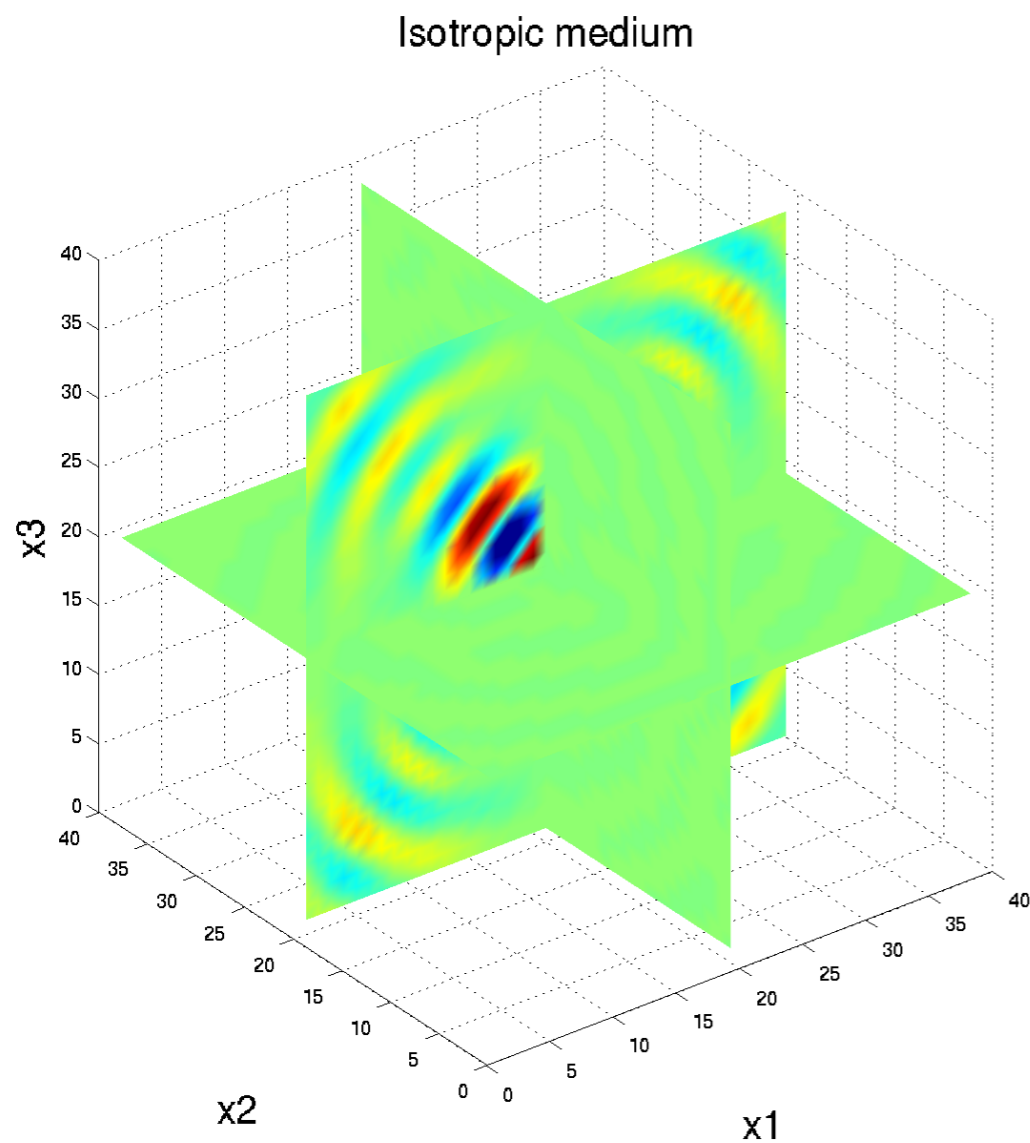


Anisotropic medium



Some results

- Medium is the same as on the previous slide
- U_2 component shown this time



Conclusion

- Constructed a staggered finite difference scheme for solving the general anisotropic visco-elastic wave equation
- Requires a low number of grid points per wavelength

Future work

- Use in full waveform inversion by inverting for all components of the (frequency dependent) stiffness tensor (or a subset)
- Optimize *current* and develop *new* preconditioners
- Investigate which combination of discretization & linear system solver & computational hardware works the fastest

Acknowledgements

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SINBAD



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